

地应力测井评价方法及其地质与工程意义

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摘要:地应力场研究可为井网部署、油气井压裂和裂缝有效性评价等提供理论指导与技术支持,系统归纳地应力场分析以及测井评价方法流程至关重要。总结了地应力场构成及其测井响应机理,并指出对地应力响应较灵敏的测井序列为声波时差、电阻率和成像测井。在声发射实验确定古构造应力场期次及大小的基础上,通过电阻率、声波时差测井和裂缝密度恢复最大古构造应力。现今地应力场一般从地应力方向和大小两个方面进行描述,确定地应力方向的测井方法是成像测井拾取井壁崩落和诱导缝、阵列声波测井横波分裂,获取地应力场大小的手段是水力压裂法和声发射实验。在现今地应力场描述的基础上,利用组合弹簧模型等模型或方法计算现今地应力大小,实现地应力场分析。地应力场分析结果有助于更好地开展断层性质分析、储层质量和裂缝有效性评价以及油气藏分布预测,此外在非常规油气储层压裂改造等工程领域也有较大的应用价值。

关键词:地应力;测井评价;断层性质;储层品质;裂缝有效性;压裂改造;非常规油气

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Well-logging evaluation of in-situ stress fields and its geological and engineering significances

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Abstract: Research of the in-situ stress field can provide theoretical guidance and technical support in well design, fracture stimulation of wells and fracture effectiveness evaluation. It is crucial to summarize the in-situ stress field analysis and related logging evaluation methods. The study summarizes the components of in-situ stress field and its well-logging response mechanism, and presents the log suite consisting of sonic transit time, resistivity and image logs as the most sensitive to in-situ stress responses. The time and magnitude of paleotectonic stress field can be determined by acoustic emission experiment. The maximum paleotectonic stress magnitude can be recovered by using resistivity log, sonic transit time log and fracture density. The in-situ stress field can be described in respect of orientation and magnitude. The orientation of in-situ stress field can be determined by using the image logs to pick up borehole breakouts and induced fractures, and the array acoustic logs to derive shear wave splitting. The magnitude of the in-situ stress field can be determined through hydraulic fracturing combined with acoustic emission experiment. The in-situ stress can be calculated through models or methods including the combined spring model built on the in-situ stress field description, realizing in-situ stress field analysis. The analytical results can better help analyze fault properties, evaluate reservoir quality and fracture effectiveness, predict reservoir distribution, as well as be of practical value to the engineering fields like hydraulic fracturing of unconventional hydrocarbon reservoirs.

Key words: in-situ stress, well-logging evaluation, fault property, reservoir quality, fracture effectiveness, hydraulic

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地应力是指地壳岩石在漫长的地质历史中形成的天然内应力^[1-5]。地应力受控于上覆岩层重力以及构造运动产生的构造应力,是岩性、埋深、岩石结构和构造的综合反映^[3,6-11]。地应力场既包括方向,也包括大小,对岩层而言,既受到垂向地应力控制,又有水平地应力影响,因此描述地应力场时应考虑地应力场方向和不同方向上的地应力大小^[12-13]。地应力研究对地质与工程均有重要的意义^[2,5-6,11,14-15]。地质上,地应力场控制了岩石的变形以及油气的运移与聚集,同时决定了储集层品质和裂缝有效性^[6,14,16-17]。工程上,地应力场对井网布置、钻完井设计和工程压裂改造至关重要^[6-8,14,18]。在非常规油气勘探开发中,水平井钻井、压裂等工程需求突出,因而地应力研究重要性凸显^[11,15,18-19]。

地应力场大小可通过地应力室内试验和矿场地应力测试等途径获取,但受到样品、矿场条件以及分析测试成本的限制,难以获得单井连续的地应力场特征变化,因而利用地球物理测井资料分析与评价地应力场分布规律成为地质与工程研究必不可少的内容^[5-6,20-21]。通过地球物理测井资料可实现古应力场的恢复,现今地应力方向判别以及现今地应力大小计算,具有纵向分辨率高、连续性好且价格低廉的优势。因此可通过测井资料来分析评价应力场方向和大小,这将为油气分布规律等地质研究提供理论指导,同时也将为开发井网布置、压裂开采措施等工程研究提供技术支撑^[5,15,19,22]。

本研究系统归纳总结了地应力场构成以及地应力场测井响应机理。古构造应力可通过声发射实验进行分析,并利用电阻率、声波时差测井和裂缝密度实现最大古构造应力测井恢复。从地应力方向和大小的角度描述现今地应力场特征,并利用声发射实验以及水力压裂法评价现今地应力场大小。依托成像测井井壁崩落和诱导缝以及声波测井横波分裂特征实现现今地应力方向判别。基于组合弹簧模型等通过声波、密度等测井资料计算由垂向应力、水平最大和最小主应力构成的三轴应力剖面。通过地应力场测井恢复与评价可分析应力状态及断层性质,为储层质量以及裂缝有效性评价提供支撑,并实现油气藏分布预测。此外,地应力场分析对于非常规油气压裂改造同样具有指导意义。研究成果能够更好地为地质与工程领域提供理论

指导与技术支持。

1 地应力场及其测井响应机理

1.1 地应力场

地应力场一般包括古应力场和现今应力场,其中,地质历史时期的构造应力场为古应力场,其结果为在岩石当中形成不同的变形和断裂形迹(褶皱、断裂和节理);现今应力场则泛指第四纪中更新世以来的地应力^[23],是古应力场的延续或继承^[14]。

对于特定地质体而言,其受到的地应力可以分解为3个相互垂直的主应力,即三轴向应力^[4],包括垂向应力、现今水平最大主应力($SH_{\max}$, MPa)和现今水平最小主应力($Sh_{\min}$, MPa),其中垂向应力主要由上覆岩层重力构成,而水平两向应力则受到岩层重力及构造挤压应力等影响^[2,6,10,15,24-28]。

1.2 地应力场测井响应机理

地应力测井评价包含两个方面的内容:①地应力场方向;②地应力大小。能够反映或评价现今地应力方向的测井序列包括成像测井、阵列声波测井、双侧向测井以及地层倾角测井,这些都是带有方位信息的测井资料^[29]。

成像测井具有分辨率高以及定向的特征,可以通过拾取井壁崩落、钻井诱导缝等特征实现地应力方向评价^[30-31]。阵列声波测井则通过探测快、慢横波方位,实现井周各向异性计算从而确定水平主应力方位^[6]。地层倾角测井可以用双井径识别井壁崩落或椭圆井眼,再结合1号极板方向确定井壁崩落方向,指示水平最小主应力方向^[5,25]。常规测井对地应力大小响应比较灵敏的主要为泥岩声波时差和电阻率测井,地应力增大导致岩石内导电孔隙流体逐渐减少,电阻率增大,而由于岩石变得致密,声波速度增加,因而声波时差变小^[6,16,20]。

目前没有直接能够测量地应力的测井序列,岩石的三轴应力往往需要通过测井曲线间接评价或计算,MDT模块式地层动态测试器,可在测试过程中测量地层压力等参数,用于刻度测井资料^[32]。

2 最大古构造应力测井恢复方法

古应力场方向可根据天然裂缝走向确定,裂缝走向分布指示古应力场活动期次,目前成像测井可以拾取天然裂缝面的形态并计算裂缝参数,因此在分析古构造应力场中应用效果显著^[33-34]。古应力大小则在实验室条件下通过岩心样品等分析测试获取,当然想要获取井段连续的古构造应力场,需要利用不同测井序列对其进行恢复。

2.1 基于声发射实验的古构造应力分析

古构造应力大小,一般可利用岩石所经历的最大古构造应力($\sigma_{\max}$, MPa)来进行表征,且 $\sigma_{\max}$ 可通过声发射实验来获得^[34-35]。声发射法是依据 Kaiser 效应而提出的古构造应力测量方法,德国科学家 Kaiser 于 1959 年发现了多晶金属具有声发射特性,即对多晶金属加载应力时,当加载的应力值达到最大应力值时材料内部会发出弹性波,并被外部接收到^[34]。在地质历史时期经历复杂构造变动的岩石同样也具有凯撒效应^[34-35],因此可通过实验获得地下岩石的 Kaiser 点,恢复地质历史时期岩石所经历的最大主应力值^[5,14,34]。需要说明的是,岩石若经历多期次构造应力场叠加改造,则在声发射实验中也可对应多个 Kaiser 点,通过 Kaiser 点个数及对应的应力值可获得应力期次及大小^[14,33,36]。

2.2 最大古构造应力测井恢复

2.2.1 泥岩声波时差与电阻率测井

可以根据岩心声发射实验获得 $\sigma_{\max}$,并建立测井曲线与 $\sigma_{\max}$ 对应关系,从而利用测井曲线计算 $\sigma_{\max}$ 。当埋藏较浅、地应力相对较弱时,即在地应力松弛地区或层段,岩石将保持较高孔隙度,此时电阻率难以反映地应力变化,但声波时差则对地应力响应灵敏。而在强挤压应力区,电阻率对地应力响应灵敏,因此可通过电阻率曲线计算地应力^[6,14,20]。

2.2.2 古应力与天然裂缝关系

天然裂缝产状、组合特征及裂缝参数往往与古构造应力场密切相关,因此可根据裂缝参数恢复古构造应力场^[37]。其中天然裂缝的产状及组合特征反映了构造应力场方向及期次,而裂缝密度等参数则与应力大小密切相关^[37-38]。古构造应力场控制了天然裂缝的形成和发育程度,但因裂缝张开度和孔隙度常受现今

应力场和成岩流体改造影响,因此通常可采用裂缝密度来反推岩石所受古构造应力大小^[25,37,39]。

3 现今地应力场方向测井评价

实验分析如波速各向异性方法(岩石中微裂缝沿垂直最大主应力方向优势分布导致不同方向上声波传播速度不同)等可以用于确定现今地应力方向^[40-41]。

目前,确定水平地应力方向的测井方法很多,最常用的方法包括:①基于声、电成像测井解释的井壁崩落法及钻井诱导缝推断法;②阵列声波测井横波分裂法(快横波方位)等;③地层倾角测井双井径曲线法^[12,30,42-44]。

3.1 井壁崩落和诱导缝

声、电成像测井可以拾取井壁崩落和钻井诱导缝,其中井壁崩落平行于 $Sh_{\min}$ 方向^[5,10,43,45-48]。在 $SH_{\max}$ 方向上,切向正应力最小,当钻井液或者泥浆柱压力较大时,该处剪切应力将变成负值,即压性应力变成张性应力,因此在该方向上的井壁会产生拉张应力,如果拉张应力超过岩石最大承受能力,则岩石破裂,产生重泥浆压裂缝。钻井过程中钻具的震动将形成细小的呈羽毛状或雁行分布的钻具振动微裂缝。对于应力比较集中的地层,钻开后构造应力将逐渐释放,产生雁列状分布的应力释放裂缝,诱导裂缝方位均指示 $SH_{\max}$ 方向^[5,10,45-46]。

3.2 横波分裂

在应力不均衡或者裂缝发育的各向异性地层中,横波传播时将分裂成快、慢横波(横波分裂)^[6,10]。由于质点垂直于水平最大地应力方向振动比沿井轴向上传播的横波速度快,因此快横波平行于 $SH_{\max}$ 方向^[15,41-42,45,48-51]。

4 现今地应力大小测井评价方法

现今地应力场除了方向外,应力大小评价同样重要^[15,18,21]。现今应力大小可以通过实验室岩心等样品测量,或由井场测试获得,同时也可依托地球物理测井资料进行计算^[15,18,21]。现今地应力大小测量方法包括:①直接测量法,包括岩心实验测量和井场测量,岩心实验测量又可分为声发射实验测定以及波速各向异性判断地应力方向,而井场测量主要是水力压裂法,可以获得水平最小主应力大小,并进一步计算得到水平最大主应力大小;②地球物理测井资料评价,通过实测资料作刻度的地球物理测井资料可以连续计算现今地

应力大小,建立连续地应力剖面^[15,18,21,25]。

4.1 井场和实验室测量

4.1.1 声发射实验确定三轴应力大小

声发射实验中的Kaiser点可以用来确定岩石古应力大小及期次^[5,40,52]。地应力声发射测试有单轴声发射和三轴声发射测试两种方法。单轴声发射实验方法是在单轴试验机上进行,并测定其单向应力,该实验岩样常在Kaiser点出现之前就发生破坏,采集到的信号不一定是Kaiser效应信号,有可能是岩样破裂信号,因此,需要增加围压,通过三轴声发射方法确定地应力。

三轴声发射地应力测试实验中,要求全直径岩心,整体连续,长度不小于15.0 cm,同时不发育宏观裂缝^[52]。在全直径岩心中,沿垂直方向选取一块柱塞样(直径2.5 cm),沿水平方向选取3块柱塞样开展三轴地应力实验,可以计算垂向、水平最大和最小地应力大小^[36]。需要说明的是,该地应力数值通常反映的也是古应力值^[44]。但由于现今应力往往是古应力值的延续与继承,因此也可通过该实验获得三轴应力值,并与测井计算的现今三轴应力场相互验证与刻度^[25,53]。

4.1.2 水力压裂法确定 $Sh_{\min}$ 大小

Fairhurst在1964年提出的水力压裂地应力测量法为应用最普遍的方法之一^[54]。当向井孔中注入流体时,会引起孔隙流体压力迅速升高,岩石发生破裂,该峰值压力对应破裂压力(p_r , MPa)。随后水力压裂裂缝将逐渐扩展,在裂缝扩展的过程中流体压力将逐渐下降,趋于稳定后的流体压力为裂缝延伸压力(p_t , MPa)。然后在裂缝扩展后一段时间内(5 min)停止注水,那么流体压力将迅速下降,然后发生小幅度反弹,反弹的峰值压力则为裂缝闭合压力(p_{FCP} , MPa),裂缝闭合压力等于 $Sh_{\min}$ ^[14,55]。

4.2 测井地应力计算

利用测井资料计算地应力具有成本低廉、资料容易获取且能够连续评价的特点^[12,21,56]。通过测井评价地应力大小的模型很多,归纳起来主要有两种:①根据井壁崩落的位置和崩落的宽度进行计算,Nikolaevskiy等^[57]和印兴耀等^[5]指出可通过成像测井求得井壁崩落宽度,进一步依据岩石力学性质,可计算最大、最小水平主应力,但由于相关的公式太复杂,而且该方法适用性不强,因此推广应用较难;②通过测井曲线计算泊松比、杨氏模量等岩石力学参数,并通过一维岩石力学模型

进行三轴应力剖面计算,该方法得到广泛应用^[18]。

4.2.1 垂向应力

20世纪初,瑞士地质学家Heim认为垂向应力主要由上覆岩层重量引起^[58]。在有连续采集的密度测井资料的情况下,垂向地应力可以很方便地求得,计算公式为:

$$S_v = \int_0^z \rho g dz \quad (1)$$

式中: S_v 为垂向应力,MPa; z 为埋藏深度,m; ρ 为岩石密度(密度测井曲线获得), kg/m^3 ; g 为重力加速度,取值 $9.8 m/s^2$ ^[27,59-60]。

4.2.2 水平两向应力大小

水平主应力有最大、最小和平均主应力之分,计算模型主要有两种模式:一种是两个水平主应力相等的单轴应变模式,主要有Heim模型^[58,61]、Matthews & Kelly模型^[62]、Terzaghi模型^[61,63]以及Anderson模型^[64]等。由于以上模式没考虑到水平构造应力的作用,不符合实际情况,这里不做重点阐述。另外一种考虑到构造应力对水平主应力影响的分层计算模式,主要有黄荣樽模型和组合弹簧模型等^[61,65]。

1) 黄荣樽模型(黄氏模型)

该模型指出水平地应力由两部分组成:①由于重力作用,水平主应力一部分为 S_v 和泊松比的函数,即 $\frac{\nu}{1-\nu} S_v$;②由构造运动所产生的附加应力,构造应力在两个方向上通常都存在,而且是不相等的^[18,65]。

黄荣樽等(1995)^[65]在进行地层破裂压力预测时建立的水平方向上的两个构造应力分量的黄氏模型在油田得到推广应用,其模型如下:

$$SH_{\max} = \left(\frac{\nu}{1-\nu} + A \right) (S_v - \alpha p_p) + \alpha p_p \quad (2)$$

$$Sh_{\min} = \left(\frac{\nu}{1-\nu} + B \right) (S_v - \alpha p_p) + \alpha p_p \quad (3)$$

式中: ν 为泊松比,无量纲; S_v 为垂向应力,MPa; p_p 为孔隙流体压力,MPa; α 为Biot弹性系数,无量纲; A 和 B 分别为最大水平应力方向和最小水平应力方向的构造应力系数,常数^[18,41]。

岩石力学参数可根据由阵列声波测井得到的纵横波时差和密度测井进行计算。因此测井资料获取的动态岩石力学参数需要与静态岩石力学参数相互刻度标定,从而提高解释的精度^[12,45,66-68]。Biot弹性系数,也称岩石孔弹性系数,通常与应力、孔隙压力密切相关,为衡量孔隙压力对有效应力作用程度的一个重要参

数^[18]。孔隙流体压力测井计算的方法有等效深度法、Bowers法、有效应力法和伊顿法等^[18,56]。

2) 组合弹簧模型

考虑到水平主应力有最大、最小之分,众多专家学者提出了组合弹簧模型^[2,15,69][公式(4)和公式(5)]。组合弹簧模型适用于构造运动比较剧烈的前陆盆地等地区,其中水平方向地应力受地质构造运动产生的构造应力影响较大。

$$SH_{\max} = \frac{\nu}{1-\nu} S_v + \frac{1-2\nu}{1-\nu} \alpha p_p + \frac{E}{1-\nu^2} \varepsilon_H + \frac{E\nu}{1-\nu^2} \varepsilon_h \quad (4)$$

$$Sh_{\min} = \frac{\nu}{1-\nu} S_v + \frac{1-2\nu}{1-\nu} \alpha p_p + \frac{E}{1-\nu^2} \varepsilon_h + \frac{E\nu}{1-\nu^2} \varepsilon_H \quad (5)$$

式中: ε_H 和 ε_h 分别为最大应力校正系数和最小应力校正系数,无量纲,可以通过实验数据和井场地应力测试分析与标定获得^[5,70-72];E为杨氏模量,GPa。

黄氏模型没有考虑最大主应力方向和最小主应力方向的应变影响,因此对于复杂应力区块地应力的计算也存在偏差。而组合弹簧模型地应力计算模型考虑了最大主应力和最小应力校正系数,因此在复杂构造区域地应力测井评价中得到广泛应用(图1)^[71-72]。

5 地应力场研究地质与工程意义

5.1 分析应力状态及断层性质

根据Anderson断层成因模式,通常在正断层形成时,最大主应力(σ_1 ,MPa)直立,中间主应力(σ_2 ,MPa)和最小主应力(σ_3 ,MPa)水平^[73]。在逆断层形成时, σ_3 直立, σ_1 和 σ_2 水平。在走滑断层形成时, σ_2 直立, σ_1 和 σ_3 水平^[2,5,27,74]。而地球物理测井资料可以分别计算三轴地应力大小,根据 S_v 、 $SH_{\max}$ 和 $Sh_{\min}$ 的大小,可以判别地层的应力状态,并进行断层属性的分析^[5,74]。

因此当测井计算的三轴应力满足 $S_v > SH_{\max} > Sh_{\min}$ 时(对应 σ_1 直立),对应正断层形成时的应力状态;当 $SH_{\max} > S_v > Sh_{\min}$ 时(对应 σ_2 直立),为走滑断层形成时的应力状态;当计算的三轴应力满足 $SH_{\max} > Sh_{\min} > S_v$ 时(对应 σ_3 直立),为逆断层形成时的应力场^[2,5,25,74]。

5.2 评价储层质量与预测油气分布

地应力场在使地下岩石变形的同时,同时还影响着流体势分布,并改变岩石孔渗性能^[6,16]。图1中不同地应力场对应的镜下观察表明,水平两向应力差较高

($\Delta\sigma = SH_{\max} - Sh_{\min}$)的层段,岩石往往易于因压实而致密,而相对水平两向应力差值较小的层段,岩石原生孔隙能得到一定程度的保留,当然部分岩石如果本身颗粒粒度细或者分选差,则抗压实能力弱,同样会被压实并变得致密^[25,51,75-76](图1)。

库车前陆盆地总体挤压应力较强,但也表现压中有张,张中有压的特征,同时在膏泥岩、煤系地层等滑脱层的影响下造就了构造样式控制下应力分布的多层次性^[20,71]。库车坳陷白垩系巴什基奇克组储集层孔隙度随着水平两向应力差与垂向应力比值($\Delta\sigma/S_v$)的增大,呈明显减小的趋势,也体现了地应力对储层孔隙度发育的影响^[6,16,75](图2)。

5.3 判断裂缝有效性

对裂缝有效性而言,古构造应力场控制了裂缝延伸方位^[34],而现今应力场则控制了裂缝张开度^[25,77]。古、今应力场的研究,对储层裂缝发育规律预测以及裂缝有效性评价具有重要意义^[32-33,78-82]。通常当裂缝的走向与现今最大水平主应力方向基本一致或夹角较小($< 30^\circ$)时裂缝张开度大,开启性好^[83-84],而与现今最大水平主应力方向有一定夹角的裂缝则有效性差^[25]。

地应力大小与裂缝参数耦合关系研究也表明, $\Delta\sigma/S_v$ 控制了裂缝有效性,随着其增大,裂缝密度和裂缝张开度均呈明显下降趋势(图3)。因此除地应力方向外,地应力大小往往也是决定裂缝有效性的重要因素^[75]。

5.4 指导非常规油气压裂改造

非常规油气藏需要钻水平井以及采取压裂改造等措施才能获得工业油气流,而压裂过程中地应力方向和大小评价至关重要^[5,11,85-88]。在压裂改造过程中,地应力场状态决定了压裂缝延伸方向,控制了压裂的增产效果。

压裂过程中,人工压裂缝易于沿着 $SH_{\max}$ 方向扩展^[15,89-90]。为了获得大体积的横切裂缝系统,水平井一般沿 $Sh_{\min}$ 方向或小于 30° 夹角钻进^[91],同时沿 $Sh_{\min}$ 方向布井。这样不仅能够有效避免井壁失稳、井塌等工程事故,而且能够沿 $SH_{\max}$ 方向压裂,提高压裂效果^[11,49]。

此外,地应力大小也是决定压裂方案设计以及压裂层段优选的重要因素,水平两向应力差在工程上影响着储层改造时裂缝的形态,两向应力差越小越易于形成复杂缝网,这对油气开采非常有利。相反,两向应力差异越大,压裂后往往形成单组裂缝,不利于非常规油气开采^[11,92](图4)。

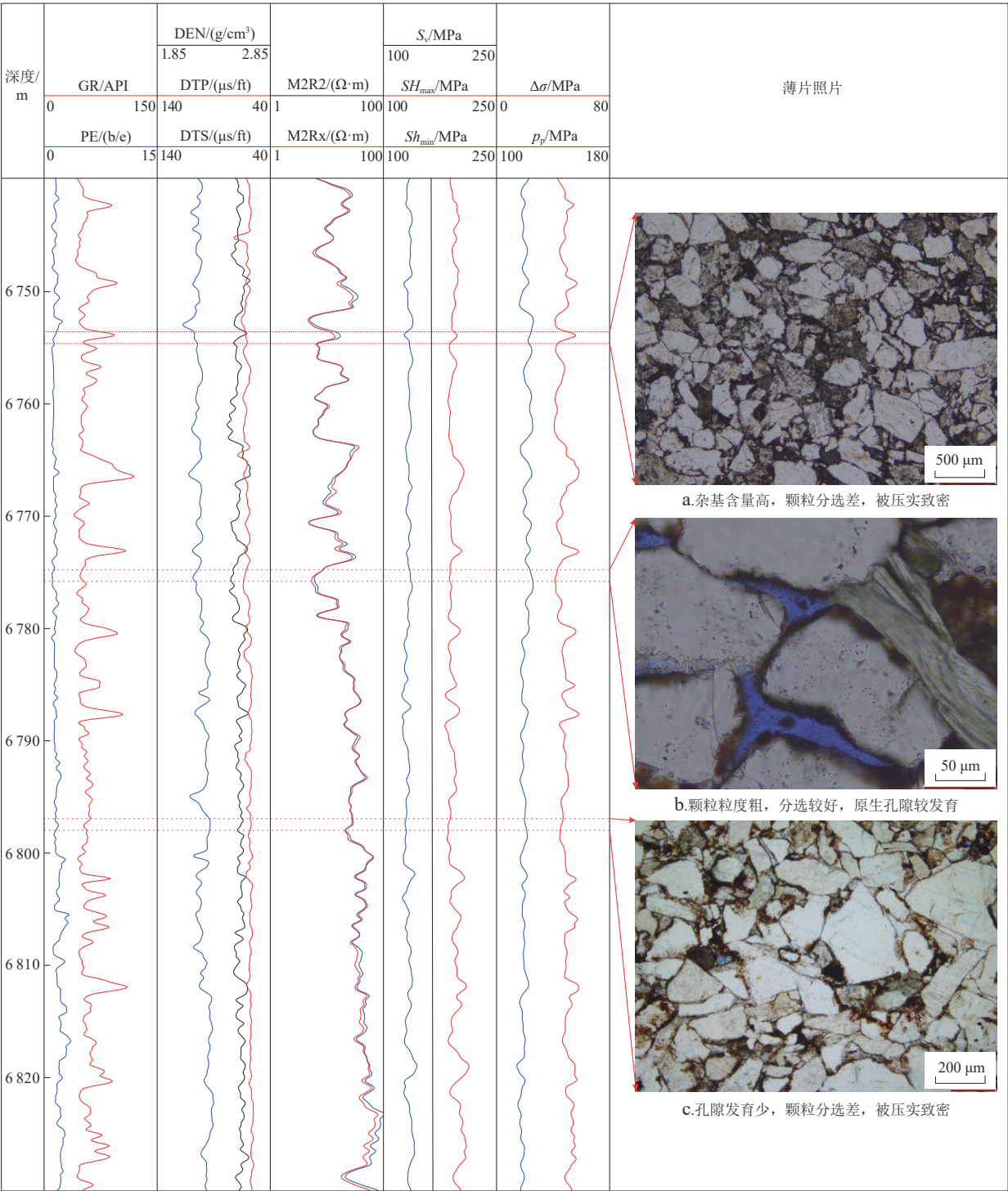


图1 塔里木盆地库车坳陷白垩系巴什基奇克组三轴应力测井评价及对应镜下薄片特征^[25]

Fig. 1 Logging evaluation of in-situ stress magnitude and related thin section images of the Cretaceous Bashijiqike Formation in Kuqa Depression, Tarim Basin^[25]

6 结论

1) 三轴应力剖面中,在最小主地应力方向上,岩石受到的剪切应力最强,最可能发生井眼崩落。在最大水平主应力方向上,井壁所受的切向应力最小,对应

诱导缝的形成。阵列声波测井横波分裂中的快横波指示水平最大主应力方向。

2) 声发射实验可获得古应力场期次及大小,而电阻率、声波时差测井和成像测井计算的裂缝密度可用于最大古构造应力测井恢复。

3) 现今应力大小可以通过实验室岩心声发射实

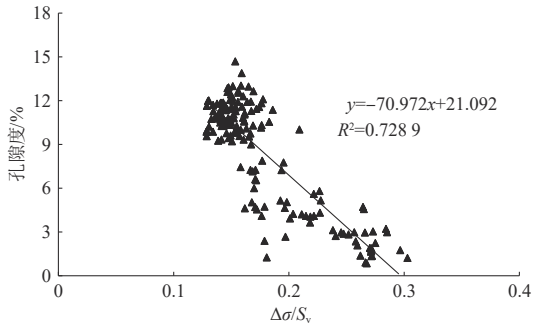


图2 塔里木盆地库车坳陷白垩系巴什基奇克组孔隙度与 $\Delta\sigma/S_v$ 关系

Fig. 2 Cross plot of porosity vs. $\Delta\sigma/S_v$ of the Cretaceous Bashijiqi reservoirs in Kuqa Depression, Tarim Basin

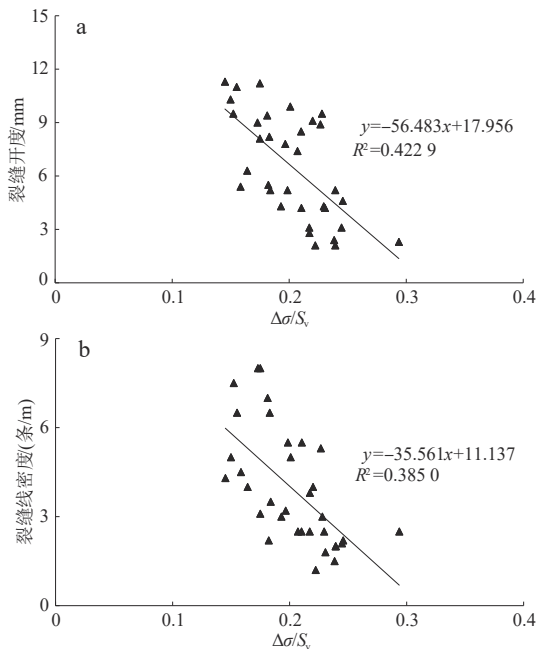


图3 塔里木盆地库车坳陷白垩系巴什基奇克组裂缝参数与 $\Delta\sigma/S_v$ 对应关系

Fig. 3 Cross plots of fracture parameters vs. $\Delta\sigma/S_v$ of the Cretaceous Bashijiqi reservoirs in Kuqa Depression, Tarim Basin

a. 裂缝开度; b. 裂缝线密度

验等测量以及水力压裂法井场测试获取,同时也可依托地球物理测井资料进行计算。垂向应力、水平最大和最小主应力三轴应力剖面可以通过组合弹簧模型等利用声波、密度等测井资料计算。

4) 地应力场研究在地质上可用于分析应力状态及断层性质,评价储层质量以及裂缝有效性。优质储层往往对应水平两向应力差值较低的层段,而与现今最大水平主应力方向平行的天然裂缝往往张开度大、有效性好。在工程上地应力场分析能够指导非常规油气压裂改造工作,水平井一般沿 Sh_{min} 方向钻进,沿最大 SH_{max} 压裂,同时优选水平两向应力差较低的层段进行压裂。

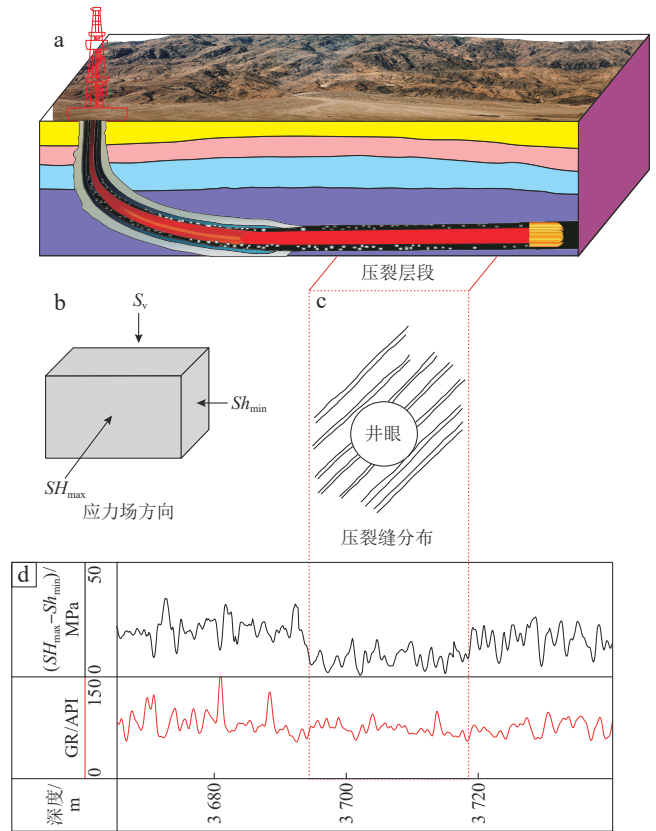


图4 水平井钻进方向、人工压裂缝形成方向及其与地应力分布关系

Fig. 4 Horizontal drilling direction, hydraulic fracture propagation and in-situ stress field in unconventional hydrocarbon reservoirs

a. 水平井井眼轨迹与地应力关系; b. 三轴应力分布特征; c. 压裂缝分布特征; d. 准噶尔盆地吉木萨尔凹陷芦草沟组压裂层段与现今地应力大小对应关系

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